







1998 IEEE AP-S International Symposium and USNC/URSI National Radio Science Meeting

Atlanta, Georgia June 21-26, 1998 Renaissance Waverly Hotel

Final Call for Papers

The 1998 URSI National Radio Science Meeting, sponsored by the USNC/URSI, and the 1998 IEEE AP-S International Symposium sponsored by the IEEE Antennas and Propagation Society (AP-S), will be held jointly at the Renaissance Waverly Hotel in Atlanta, Georgia, 21-26 June 1998. The technical sessions, workshops, and short courses will be coordinated among the two symposia to provide a comprehensive and well-balanced program.

★ Electronic Paper Submission **★**

The 1998 IEEE AP-S/URSI Symposium in Atlanta will mark the first use of electronic paper submission by the USNC and the AP. Society. In addition, the conference digests will be placed on an archival CD-ROM with a fully indexed and searchable system for fast document retrieval. For the first time in the history of this conference, authors will be able to submit their work with full color illustrations and figures and attendees will be able to search the CD based on topic keyword and author name! Authors should visit the Symposium homepage and the Technical program Committee (TPC) web page for detailed information on how to take full advantage: of available technology when submitting a paper.

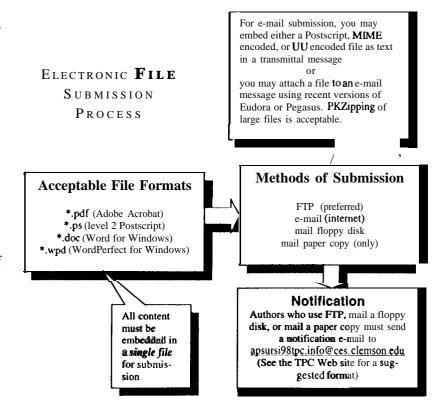
To guard against the hazards of the electronic age and electronic submission, all summaries and abstracts must also be submitted in paper form by 19 January 1998 to Wilson Pearson's address listed herein. The paper copy will be used for backup purposes in the event that an author's electronic copy is unusable.

Detailed Information. To assist authors in the preparation and submission of the electronic copy of their summary or abstract, several information sources will be available. Information may be obtained from the Technical Program Commit tee web site: http://apsursi98tpc.ces.clemson.edu. Information may be obtained via FTP by downloading an Adobe Acrobat file (submission.pdf) or a text file (submission.txt) from apsursi98tpc.ces.clemson.edu. Finally, one may send e-mail with the subject Submission to apsursi98tpc.info@ces.clemson.edu to generate an automatic reply message containing full details on preparation and submission.

For those who cannot comply. It is expected that a very small number of authors will be unable to generate an electronic copy of the summary or abstract. These authors must submit one original and three copies of their contribution, along with the completed copyright form, to Wilson Pearson at the address given by 5 January 1998.

Interactive Forum

An Interactive Forum will be held daily during the first three days of the Symposium and Meeting. The space provided for forum presentations will include approximately forty square feet of tackboard space, a table, and access to electrical power if needed. The forum



will be located in an open central public area of the meeting. Consequently, the interactive forum vehicle provides an alternative to

podium presentations that lends itself to better exposition of many results. For example, the large display area provides the means for comparative display of a large number of charts for results-intensive presentations. The table and power provide the means for interactive computer presentations. Authors are encouraged to take advantage of this format in a creative fashion, The best use of the Interactive Forum will be recognized at the Awards Banquet. Authors are asked to designate their desire to participate in an interactive forum at the time they submit their papers.

Instructions for all Authors

The e-mail or letter accompanying the summary (for AP-S) or abstract (for USRI) must indicate a topic number associated with AP-S or URSI from the tabulation elsewhere in this Call. Papers submitted for the student paper competition should be so designated and comply with instructions below. It must contain the complete mailing address, telephone number, e-mail address, and fax number of the corresponding author. Where there are multiple authors, specify the presenter by an asterisk. Authors desiring placement in an interactive forum should indicate this in their transmittal. The presentation equipment needed (viewgraph, 35 mm slide projector, etc.) should be also be specified.

The language of the conference is English. Simultaneous interpretation will not be provided. The text should be formatted single spaced and sized for 21.5 x 28-cm (8.5 x 11 inch) paper. The title should be centered 1 inch from the top of the first page. The author's (or authors') name and complete organizational affiliat ion should be two lines below the title. The text should start three lines below the last name. Left and right-hand margins should be 4 cm (1.5 inches). A 2.5-cm (1-inch) margin should be at the top and bottom of all pages. Double space between paragraphs. Submissions must withstand a linear reduction to 70% of original size and maintain readability y. Only the corresponding author will receive an acknowledgement of the submission. FAX SUBMISSIONS WILL NOT BE ACCEPTED.

Additional Instructions for AP-S Authors

The summary must be limited to four pages including text, references, figures, and photographs. The introduction should indicate clearly how the submission relates to previous work and the unique aspects of the current submission. One paper copy and one **electronic** copy (see Mow) of the summary must be submitted in final form. Figures and photographs (in glossy prints) should be a convenient size and affixed on 21.5 x 28-cm (8.5 x 11) white paper with captions typed in appropriate places. Footnotes should not be used except for credits to sponsoring agencies. A signed copyright form is necessary with submission of the paper copy (forms are in recent issues of the IEEE Transactions on Antennas & Propagation and available through the **homepage**). Missing copyright forms will make it necessary to reject the paper. It will be understood that all submissions have been cleared by the sponsoring agency.

Additional Instructions for URSI Authors

The abstract must consist of at least 250 words, and must be limited to one page, including figures. One paper copy and one electronic copies of the abstract must be submitted in final form. Do not include a list of references, a few open literature references may be included parenthetically, for example (R. L. Lewis and J. R. Johler, Radio Sci., 2, 75-81, 1976). Acknowledgement of financial support is not deemed appropriate.

Provide an accompanying second page that includes (1) identification of Commission and session topic for the paper (2) a statement of what new knowledge is contributed by this paper, and (3) the relationship of this work to previous work.

AP-S Student Paper Competition

A student paper contest for full-time students will be held as part of the symposium. To be considered, a student must be the first author of the paper. The student's advisor should attach a statement that his/her contribution is primarily advisory. In addition, e-mail notification (or transmittal letter) should clearly indicate student paper submission and conform to all other submission requirements as delineated above. Student papers judged as finalists will be presented at the conference in the interactive forum format.

Submission Addresses

Submit electronic form of documents via one of the following mechanisms:

FTP: apsursi98tpc.ces.clemson.edu e-mail: apsursi98tpc@ces.clemson.edu

FTP is preferred if you have access to the capability.

Submit paper copy and copyright form to L. Wilson Pearson
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Deadlines

For authors submitting electronic copy, the deadline for the receipt of it is 12 January 1998. The deadline for the corresponding backup paper copy is 19 January 1998. For authors who cannot comply, the paper-copy deadline is 5 January 1998. "All deadlines will be adhered to strictly.

Web Addresses

http://seal.gatech.edu/EEED/AP-URSI98/ap-ursi98.htm

http://apsursi98tpc.ces.clemson.edu

(Symposium homepage) (TPC Information homepage)

Authors are invited to submit papers of interest to the AP-5 membership and to the following URSI commissions:			
AP-S S	special Sessions (These sessions will comprise, in part, invite	ed speak	ers, but contributions are welcomed.)
AP-1	Keynote Session: The Next Generation of Communications Satellites	AP-5	Session Honoring Prof. T. B. A. Senior
AP-2	Keynote Session: The Next Generation of Communications Satellites—Antennas, the Enabling Technology	AP-6 S	Session Honoring Prof. R. E. Collin
AP-3	Keynote Session: Wireless (Terrestrial) Networks	AP-7	Equivalence Principle
AP-4	Keynote Session: Measurements	(AP-8)	Spatial Power Combining of mmW Radiation
AP-S General Sessions			
AP-9	Adaptive, active, signal processing & imaging antennas	AP-24	Microstrip antennas, arrays, and circuits ."
AP- 10	Biomedical Applications	AP-25	Monolithic array techniques
AP-11	Broadband and multifrequency antennas	AP-26	Phased array antennas
AP- 12	Mobile and PCS antennas	AP-27	Applications of Photonics in antenna systems
AP- 13	Electromagnetics Education	AP-28	Digital beamforming
AP- 14	Electromagnetic properties of materials	AP-29	Non-linear electromagnetic
AP-15	Electromagnetic theory ,, .	AP-30	Optimization methods in EM design ,
AP- 16	Frequency selective surfaces /	AP-31	Neural networks
AP-17	FEM methods	AP-32	Reflector antennas
AP-18	FDTD methods :	AP-33	Scattering, diffraction and radar cross security
AP-19	Wavelet-based methods	AP-34	Radar imagery
AP-20	Transients and time domain techniques	AP-35	Propagation
AP-21	Numerical methods	AP-36	
AP-22	Numerical methods Inverse scattering	AP-37	
AP-23	inverse scattering	AP-38	Other topics
AF-23	Waveguiding structures ,,	Ar-30	Officer topics , , , , , , , , , , , , , , , , , , ,
COMMISSION A, Electromagnetic Metrology			
A-1 General			
A-1	General		
	MISSION B, Fields and Waves		
B-1	Novel Methods (Special Session)	B-9	Numerical methods (differential equations)
B - 2	Antennas	B-10	Numerical methods (integral equations)
B-3	Arrays	B-n	Numerical techniques (hybrid and other),'
B-4	Complex media	B-12	Rough surfaces and random media
B-5	Guided waves	B-13	Scattering
B-6	High frequency techniques	B-14	Theoretical electromagnetic
B-7	inverse scattering	B-15	Transient fields, effects, and systems
B-8	Microstrip lines, antennas, and circuits		
COMMISSION D. Electronics and Photonics			
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	IISSION D, Electronics and Photonics Microelectromechanical Systems MEMS	D-5	Microwave millimeter wave and submillimeter wave
COMM D-1	Microelectromechanical Systems, MEMS	D-5	Microwave, millimeter wave, and submillimeter wave
D-1	Microelectromechanical Systems, MEMS (Special Session)		devices and circuits
D-1 D-2	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials	D-6	devices and circuits High speed devices and circuits
D-1 D-2 D-3	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits	D-6 D-7	devices and circuits High speed devices and circuits Mesoscale devices and associated materials
D-1 D-2	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials	D-6	devices and circuits High speed devices and circuits
D-1 D-2 D-3 D-4	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection	D-6 D-7	devices and circuits High speed devices and circuits Mesoscale devices and associated materials
D-1 D-2 D-3 D-4 COMM	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection ISSION F, Wave Propagation and Remote Sensing	D-6 D-7 D-8	devices and circuits High speed devices and circuits Mesoscale devices and associated materials Vacuum microelectronics
D-1 D-2 D-3 D-4 COMM F-1	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection ISSION F, Wave Propagation and Remote Sensing Terrestrial Propagation Effects (Model and Mess.)	D-6 D-7 D-8	devices and circuits High speed devices and circuits Mesoscale devices and associated materials Vacuum microelectronics Indoor Propagation (Model and Measurements)
D-1 D-2 D-3 D-4 COMM	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection ISSION F, Wave Propagation and Remote Sensing	D-6 D-7 D-8	devices and circuits High speed devices and circuits Mesoscale devices and associated materials Vacuum microelectronics
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D-1 D-2 D-3 D-4 COMM F-1 F-2	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection ISSION F, Wave Propagation and Remote Sensing Terrestrial Propagation Effects (Model and Mess.) Satellite-Earth Propagation (Model and Measurements)	D-6 D-7 D-8	devices and circuits High speed devices and circuits Mesoscale devices and associated materials Vacuum microelectronics Indoor Propagation (Model and Measurements)
D-1 D-2 D-3 D-4 COMM F-1 F-2 COMM	Microelectromechanical Systems, MEMS (Special Session) Optoelectronic techniques, devices, and materials Cryogenic electronic devices and circuits Optical transmission and interconnection ISSION F, Wave Propagation and Remote Sensing Terrestrial Propagation Effects (Model and Mess.) Satellite-Earth Propagation (Model and Measurements) ISSION K, Electromagnetic in Biology and Medicine	D-6 D-7 D-8 F-3 F-4	devices and circuits High speed devices and circuits Mesoscale devices and associated materials Vacuum microelectronics Indoor Propagation (Model and Measurements) Mobile Propagation (Model and Measurements)

Authors are invited to submit papers of interest to the AP-S membership and to the following URSI commissions:

The Dynamics of Coupled Oscillator Phase Control

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Arrays of coupled oscillators have been proposed as means of realizing high power rf sources via coherent spatial power combining.[1][2] In such applications, a uniform phase distribution over the aperture is usually desired. However, it has been shown that by detuning some of the oscillators away from the oscillation frequency of the ensemble of oscillators, one may achieve other useful aperture phase distributions. [3] Of particular interest among those achievable are linear phase distributions because these result in steering of the output rf beam away from the broadside direction. The theory describing the behavior of such arrays of coupled oscillators is quite complicated since the phenomena involved are inherently nonlinear. However, a simplified theory has been developed which facilitates intuitive understanding. [4] This simplified theory is based on a "continuum model" in which the aperture phase is represented by a continuous function of the aperture coordinates. A challenging aspect of the development of this theory is the derivation of appropriate boundary conditions at the edges or ends of the array.

We begin by reviewing the nonlinear equations describing the behavior of an array of loosely coupled oscillators. [2] The behavior of the phase of a single oscillator injection locked to an input signal,

$$V_{n,j} = A_{inj} e^{j(\omega_{inj}t_1 \cdot (\cdot, \cdot, \cdot, \cdot))} = A_{inj} e^{j\theta_{inj}}$$

$$\tag{1}$$

can be described by the following differential equation.

$$\frac{d\theta}{dt} = \omega_o - t \Delta \omega_{lock} \sin(\theta_{inj} - \theta)$$
 (2)

where $\theta = \omega t + \phi$, ϕ is the phase of the oscillator oscillating at frequency, ω ,

$$\Delta\omega_{lock} = \frac{\omega_o}{2Q} \frac{A_{inj}}{A} \tag{3}$$

the locking bandwidth which is inversely proportional to the Q of the oscillator and A, the amplitude of the oscillation. For a linear array of N coupled oscillators, the **injection** signals are just the outputs of the other oscillators and the phase of the i^{th} oscillator is described by a differential equation of the form,

$$\frac{de_{i}}{dt} = \omega_{o} - \frac{\omega_{i}}{2} \sum_{j=1}^{N} \varepsilon_{ij} \frac{A_{j}}{A_{i}} \sin(\Phi_{ij} + \theta_{i} - \theta_{j})$$
(4)

and $\varepsilon_{ij}e^{j\Phi_{ij}}$ is the coupling between oscillators i and j. This system of equations, one equation for each value of i, has a coefficients matrix with zero determinant, a manifestation of the arbitrary nature of the phase reference. York has suggested that this may be remedied by dealing with phase differences between neighboring oscillators. Thus, we write,

$$\frac{d(\Delta\phi_i)}{dt} = (\omega_{tune,i+1} - \omega_{tune,i}) - \Delta\omega_{lock,ij} \sum_{\substack{j=i+1\\j=i-1}} (\Delta\phi_i - \Delta\phi_j)$$
 (5)

where,

$$\Delta \phi_i = \phi_{i+1} - \phi_i \to \frac{\partial \phi}{\partial x} = \widetilde{\psi} \tag{6}$$

the phase gradient. Consider an infinitely long linear array in which the center oscillator tuning frequency is increased by an amount C from the ensemble frequency at t=O. Limiting the coupling to nearest neighbors and taking the continuum limit (i becomes a continuous variable, x), results in,

$$\frac{\partial^2 \widetilde{\psi}}{\partial x^2} - \frac{\partial \widetilde{\psi}}{\partial \tau} = -\frac{1}{\Delta \omega_{\text{turk}}} \frac{\partial \omega_{\text{turk}}}{\partial x} = -Cu(\tau)\delta'(x) \tag{7}$$

where $\Delta\omega_{lock}$ is the mutual locking bandwidth of the coupled oscillators and includes the magnitude of the coupling constant, ϵ_{ij} , τ is time multiplied by the locking bandwidth, while $\omega_{lune}(x)$ gives the oscillator tuning frequencies. This equation may be solved via Laplace transformation with respect to time resulting in,

$$\phi(x,\tau) = C \left[2\sqrt{\frac{\tau}{\pi}} e^{-\frac{x^2}{4\tau}} - |x| \operatorname{erfc}\left(\frac{|x|}{2\sqrt{\tau}}\right) \right] u(\tau)$$
 (8)

Note that this diverges as **the** square root of **time** as **time** approaches infinity. However, the frequency function, obtained by time differentiation, converges to the original ensemble frequency as one over the square root of time which is consistent with the fact that detuning one of the infinite number of oscillators does not change the ensemble frequency; i.e., the average of the tuning frequencies.

Consider now a finite length array extending from -a to a along x. The boundary conditions are derived by writing the equations of (5) for the oscillators at the ends of the array and proceeding to the continuum limit. This leads to.

$$\frac{\partial \widetilde{\psi}}{\partial \tau}\Big|_{-\left(a-\frac{1}{2}\right)} = \frac{1}{\Delta \omega_{lock}} \frac{\partial \omega_{tune}}{\partial x}\Big|_{-\left(a-\frac{1}{2}\right)} + \frac{\partial \widetilde{\psi}}{\partial x}\Big|_{-\left(a-1\right)} \cdot \widetilde{\psi}\Big|_{-\left(a-\frac{1}{2}\right)}$$
(9)

$$\frac{\partial \widetilde{\psi}}{\partial \tau} \Big|_{\left(a-\frac{1}{2}\right)} = \frac{1}{\Delta \omega_{lock}} \frac{\partial \omega_{turk}}{\partial x} \Big|_{\left(a-\frac{1}{2}\right)} \frac{\partial \widetilde{\psi}}{\partial x} \Big|_{\left(a-1\right)} - \widetilde{\psi} \Big|_{a-\frac{1}{2}\right)} \tag{lo}$$

s o 1 v i n g (7) with these boundary conditions via Laplace transformation and integrating the resulting expression for the phase gradient gives the following for the transform of the aperture phase distribution.

$$f(x,s) = \frac{C}{2s^2} \left\{ \frac{\left(s+I\right)\cosh\left[\sqrt{s}\left(a-\frac{I}{2}-|x|\right)\right] + \sqrt{s}\sinh\left[\sqrt{s}\left(a-I-|x|\right)\right]}{\cosh\left[\sqrt{s}\left(a-I\right)\right] + \frac{s+I}{\sqrt{s}}\sinh\left[\sqrt{s}\left(a-\frac{I}{2}\right)\right]} \right\}$$
(11)

This can be inverted via the calculus of residues in the form,

$$\phi(x,\tau) = \left[\frac{C\tau}{2a+1} + r_{-1} + \sum_{n=0}^{\infty} r_n e^{-\sigma_n \tau} \right] u(\tau)$$
 (12)

where,

$$6 = \frac{C}{2(2a+1)} \left[\frac{(2a+1)}{2} - |x| \right]^2 + K$$
 (13)

indicating that the steady state frequency is shifted to the new average of the oscillator tuning frequencies and that the steady

state phase distribution is quadratic. Figure 1 shows typical space-time behavior of the aperture phase of a finite array obtained from (12).

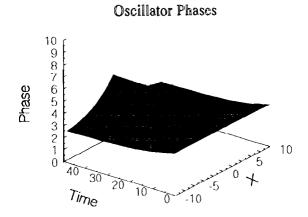


Figure 1. **Typical** space-time behavior of the phase of a finite length linear array of oscillators under step detuning of the center oscillator.

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- 1. J. W. Mink, "Quasi-optical power combining of solid-state millimeter-wave sources," IEEE Trans. Microwave Theory Tech., vol. MTT-34, pp. 273-279, Feb. 1986.
- 2. R. A. York, "Nonlinear Analysis of Phase Relationships in Quasi-Optical Oscillator Arrays," IEEE Trans. . Microwave Theory Tech., vol. MTT-41, pp. 1799-1809, Oct. 1993. [See also references therein.]
- 3. P. Liao and R. A. York, "A New Phase-Shifterless Beam-Scanning Technique Using Arrays of Coupled Oscillators," IEEE Trans. . Microwave Theory Tech., vol. MTT-41, pp.1810-1815, Oct. 1993.
- 4. R. J. Pogorzelski and R. A. York, "A Simplified Theory of Coupled Oscillator Phase Control," IEEE AP-S International Symposium, Montreal, Quebec, July 1997.